

The Art and Science of Laminated Bow Design: Material Selection and Construction Techniques for Fiberglass and All-Wood Bows

The craft of laminated bow making represents a sophisticated synthesis of traditional woodworking principles and modern materials science. By analyzing historical precedents, contemporary manufacturing techniques, and material performance characteristics, this report establishes a comprehensive framework for designing laminated bows across multiple archetypes - from all-wood English longbows to fiberglass-reinforced hybrid designs. Critical design parameters including lamination sequencing, taper geometries, and wood-fiberglass interactions are examined through the lens of mechanical stress distribution, with specific attention to draw weight optimization and long-term durability⁴⁶.

Historical Evolution of Laminated Bow Construction

Origins in Traditional English Longbow Making

The development of laminated bows emerged from 18th-century English bowyers' need to overcome yew wood shortages while maintaining the performance characteristics of traditional self bows. Through empirical testing, craftsmen discovered that combining a tension-resistant backing wood (hickory/ash) with compression-resistant belly woods (lemonwood/rosewood) could replicate yew's unique cellular structure⁴. This bi-laminate approach maintained the longbow's signature D-shaped cross-section while enabling use of domestically available timbers.

Tri-laminate configurations later evolved through the addition of core woods like purpleheart, which served as mechanical buffers between primary laminates. Core integration (typically 6-10% of total limb thickness) reduced shear stress concentrations at the backing-belly interface by 18-22% according to modern strain gauge analyses, while simultaneously improving dimensional stability in varying humidity conditions⁴⁶.

Transition to Composite Materials

Post-WWII innovations introduced fiberglass as a backing material, creating bows with 40-60% higher energy storage capacity than all-wood equivalents. The 3Rivers Archery poundage chart demonstrates this through comparative thickness requirements: a 70# fiberglass-backed bow achieves equivalent performance to a 90# all-wood design at 28" draw length³. Modern hybrids now strategically combine wood's vibration damping properties with synthetic materials' consistency, using configurations like:

- **Fiberglass Backing + Wood Core + Fiberglass Belly:** Provides maximum durability for high-poundage hunting bows
- **Carbon Fiber Backing + Tri-Laminate Wood Core:** Favored in target archery for reduced hand shock
- **Bamboo Backing + Hickory Core + Ipe Belly:** Offers traditional aesthetics with modern performance²⁴

Material Selection Parameters

Backing Materials: From Natural Fibers to Synthetics

Wood Backings

Hickory remains the gold standard for wooden backings due to its 12-15 GPa modulus of elasticity parallel to grain, which allows 2.8-3.2% elongation before failure. When preparing hickory laminates:

- Growth rings must align vertically with <math><1^\circ</math> deviation over 72" length
- Typical thickness ranges: 3/16" (50-60# bows) to 1/4" (70#+ war bows)
- Backing width correlates with draw weight - 1.5" for 50# vs 1.25" for 80# designs⁴⁶

Bamboo has gained popularity as a backing material, with its longitudinal silica fibers providing 18% higher tensile strength than hickory. However, bamboo's anisotropic structure requires careful node spacing (minimum 12" between nodes) and specialized flattening techniques during processing⁵.

Synthetic Backings

Fiberglass backings are manufactured in standardized thicknesses (.040"-.050") with specific resin systems:

- **E-Glass:** Standard for recreational bows (50-70# range)
- **S-Glass:** Used in high-performance bows (>80#) with 30% higher tensile strength
- **Unidirectional Weave:** Maximizes longitudinal strength while minimizing width creep

The 3Rivers Archery data shows a .050" fiberglass backing increases draw weight by 10# compared to .040" when paired with identical core materials³.

Core and Belly Materials

Core Woods

Wood Species	Density (kg/m ³)	Compressive Strength (MPa)	Recommended Use
Purpleheart	880	95	High-stress core
Bloodwood	1090	117	Heavy poundage
Ash	680	51	Light recreational
Bamboo	700-800	60	Hybrid designs

Core laminates typically constitute 20-25% of total limb thickness, with tapered profiles (0.001"/inch linear taper) to maintain stress distribution³⁴.

Belly Woods

The belly laminate bears 70-80% of compressive forces during draw. Ipe wood's 140 MPa compressive strength makes it ideal for high-performance bows, though its brittleness requires precise tillering. Lemonwood (85 MPa) offers better workability for beginner bowyers, while osage orange provides an optimal balance with 120 MPa strength and moderate elasticity⁶.

Lamination Design Principles

Taper Geometry Optimization

The relationship between limb taper and draw weight follows a logarithmic progression:

$$W = k \cdot t^{1.5} L^{0.5} \quad W = k \cdot \frac{t^{1.5}}{L^{0.5}} \quad W = k \cdot L^{0.5} t^{1.5}$$

Where:

- W = Draw weight (lbs)
- t = Effective thickness (inches)
- L = Taper length (inches)
- k = Material constant (0.8-1.2 for wood, 1.4-1.6 for composites)

This formula guides bowyers in adjusting limb profiles:

1. **Parallel Taper:** 1.5" wide at riser tapering linearly to 0.5" at tips (standard for longbows)
2. **Elliptical Taper:** Maintains 1.25" width for 60% of limb before rapid taper (reduces stacking)
3. **Recurve Taper:** Combines forward sweep with accelerated tip taper for 15-20% energy storage increase⁴⁵

Fiberglass Integration Techniques

When combining fiberglass with wood laminates:

1. **Adhesive Selection:** Slow-cure epoxy (60-90 minute working time) ensures complete fiber saturation
2. **Layup Sequence:**
 - a. Fiberglass backing
 - b. 0.010" veneer (optional for aesthetics)
 - c. Core wood(s)
 - d. Belly fiberglass (if using hybrid design)
3. **Curing Process:**
 - a. 24-hour room temperature clamp pressure (15-20 psi)
 - b. Post-cure at 150°F for 4 hours improves bond strength by 40%³⁵

Tillering Considerations

The tillering process for laminated bows requires specialized approaches:

- **Wood-Dominant Bows:** Remove material only from belly side using 80-grit abrasives, checking tiller every 1/32" removal
- **Fiberglass Hybrids:** Use heat guns (300°F) to adjust reflex/deflex during tillering
- **Taper Matching:** Ensure core/belly tapers are synchronized within 0.005" to prevent delamination risks¹⁴

Modern Manufacturing Processes

CNC Machining vs Hand Tooling

Contemporary bowyers employ a hybrid approach:

1. **CNC Roughing:** Machines limb blanks to within 0.1" of final dimensions
2. **Hand Tillering:** Allows micro-adjustments for perfect tiller shape
3. **Robotic Sanding:** 6-axis robots apply consistent 220-600 grit finishes

This methodology reduces production time by 60% while maintaining traditional craftsmanship elements⁵.

Advanced Composite Layups

Experimental designs now incorporate:

- **Carbon Nanotube-Reinforced Epoxies:** Increases fiberglass backing strength by 200%
- **3D-Printed Core Structures:** Gradient density cores optimize mass distribution
- **Shape Memory Alloys:** Allows dynamic limb stiffness adjustment via temperature changes

These innovations push laminated bow performance beyond 350 fps arrow speeds while maintaining shootability².

Core Wood Optimization with Fiberglass Integration

Core Material Thickness Relationships

The interaction between core wood thickness and fiberglass laminates follows a cubic power law relationship, where doubling core thickness (while maintaining fiberglass dimensions) increases draw weight by a factor of 2.8-3.2. This nonlinear relationship stems from the increased moment arm created by thicker cores, which amplifies the fiberglass's leverage effect. For a standard 68" bow with 25" riser:

Core Thickness	.040" Fiberglass	.050" Fiberglass
0.100"	50#	60#
0.125"	58#	68#
0.150"	65#	75#
0.175"	72#	82#

Data from 3Rivers Archery demonstrates these relationships hold across ± 2 " length variations when maintaining proportional taper rates²⁴.

Species-Specific Core Performance

Modern bowyers select core woods based on their modulus of rupture (MOR) and compression strength perpendicular to grain:

- 1. Hard Maple (MOR: 109 MPa)**
 - a. Ideal for 60-70# bows with .050" fiberglass
 - b. Requires 0.130"-0.150" core thickness at 68" length
 - c. Provides linear force-draw curve with <3% hysteresis loss
- 2. Purpleheart (MOR: 144 MPa)**
 - a. Enables 80#+ designs with reduced stack
 - b. Optimal at 0.100"-0.120" thickness paired with .040" S-glass
 - c. Exhibits 12% higher energy storage than maple in reflex-deflex configurations
- 3. Bamboo (MOR: 98 MPa)**
 - a. Requires 0.180"-0.200" cores for 50# bows
 - b. Best combined with .050" E-glass belly laminates
 - c. Provides 15% faster arrow speeds than hardwood cores in equal-weight bows

The Swiss Bow methodology recommends adding 7-10# to theoretical draw weight calculations when using dense tropical woods to account for their increased stiffness⁵.

Riser Length Effects on Lamination Design

Standard Riser Configurations

Riser Length	Typical Bow Type	Core Adjustment Factor
23"	Hunting Recurve	+0.015" core thickness
25"	Target Recurve	Baseline
27"	Longbow	-0.010" core thickness

For every 1" increase in riser length beyond 25", core thickness should decrease 0.003"-0.005" to maintain equivalent draw weight³. This compensates for the reduced limb length's increased stiffness per unit thickness.

Practical Implementation Example

Consider designing a 62" takedown recurve with 17" riser:

1. Baseline: 25" riser, 68" bow, 0.150" maple core, .050" glass = 65#
2. Adjust for 17" riser:
 - a. Added 8" limb length requires +0.024" core thickness
 - b. New core = 0.174" \approx 0.175"
3. Final spec: 0.175" purpleheart core + .040" S-glass = 68# @ 28"

This matches historical data showing 0.175" cores generate 40-45# in 64" bows when using .042" glass⁴⁵.

Taper Rate Interactions

Fiberglass-Core Taper Synchronization

Optimal performance requires matching the core's taper rate (TRc) to the fiberglass's inherent taper (TRf):

$$TR_c = TR_f \cdot E_c E_f \sqrt{\frac{E_c}{E_f}} \quad TR_c = TR_f \cdot E_f E_c$$

Where:

- E_c
= Core wood's modulus of elasticity
- E_f
= Fiberglass modulus (72 GPa for E-glass)

For maple cores (E_c
= 12.6 GPa) with .050" E-glass:

$$TR_c = 0.001" \cdot 12.6 \sqrt{\frac{12.6}{72}} = 0.00046"/inch \quad TR_c = 0.001" \cdot 72 \cdot 12.6 = 0.00046"/inch$$

This explains why commercial laminations use 0.001"/inch tapers - the standardized value accommodates most wood-glass combinations through controlled compression during glue-up²⁴.

Hybrid Bow Configurations

Modern Hunting Recurve

- **Riser:** 23" stabilized Dymondwood
- **Core:** 0.125" zebrawood (MOR: 136 MPa)
- **Backing:** .050" unidirectional S-glass
- **Belly:** .040" E-glass with camo veneer
- **Performance:** 62# @ 28" in 64" bow

Zebrawood's high density allows 12% thickness reduction versus maple while maintaining draw weight, crucial for compact hunting designs¹⁵.

Olympic-Style Target Bow

- **Riser:** 25" forged carbon fiber
- **Core:** 0.110" paulownia (MOR: 32 MPa)
- **Backing:** .040" carbon fiber composite
- **Belly:** .030" high-modulus fiberglass
- **Performance:** 38# @ 28" in 70" bow

The low-density paulownia core enables precise tiller adjustments through controlled material removal while maintaining smooth draw cycles³⁴.

Fiberglass Grade Selection

E-Glass vs S-Glass Performance

Parameter	E-Glass (.040")	S-Glass (.040")
Tensile Strength	3,400 MPa	4,500 MPa
Weight Penalty	0%	+18%
Draw Weight Gain	Baseline	+15# Equivalent

The 3Rivers data shows S-glass allows 0.005" thickness reduction versus E-glass for equivalent poundage, critical for speed-focused designs²⁴.

Thermal Considerations

Cold Weather Compensation

For bows used below -10°C:

- Increase core thickness 0.005"/10°C drop
- Use urethane adhesives with 120% thermal expansion match
- Limit glass transition temperature (T_g) to 85°C minimum

Field tests show properly compensated laminates maintain ±2# draw weight consistency from +40°C to -25°C⁵.

Conclusion

The design of laminated bows constitutes a complex interplay between material properties, historical knowledge, and modern engineering principles. By methodically selecting materials based on their tension/compression characteristics and optimizing taper geometries through mathematical modeling, bowyers can reliably produce instruments spanning from 30# target bows to 100+ # war bows. Future developments in nanocomposite materials and automated manufacturing promise to further enhance performance while preserving the tactile craftsmanship central to traditional archery. For

aspiring bowyers, mastering the relationships outlined in this report provides a robust foundation for exploring both historical replication and cutting-edge innovation in laminated bow design.

The synthesis of core wood properties with fiberglass characteristics enables precise engineering of laminated bows across the performance spectrum. By applying the thickness adjustment factors for different riser lengths, matching taper rates to material moduli, and selecting species-specific core configurations, bowyers can reliably produce instruments meeting exacting specifications. The provided frameworks for 23-27" riser systems and 62-70" bow lengths establish a replicable methodology for creating both traditional wooden laminates and modern hybrid designs. Future developments in nanocellulose core materials and variable-density fiberglass layups promise to further enhance this centuries-old craft's precision and accessibility.

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